

Lecture Superconducting Power Systems Winter term 2022/2023 Basics of Cryogenics Mathias Noe

Institute for Technical Physics (ITEP)





Contents

Motivation

Refrigerators

Cryostats

2

Application Examples

3



What effort is required to cool back a heat output of 1 W at low temperatures?

Carnot efficiency of refrigerators

$$\eta_{c,77\ K} = \frac{T_k}{T_w - T_K} = \frac{77\ K}{300\ K - 77\ K} = \frac{77\ K}{223\ K} = 0.3453$$

$$2.9\ W$$

$$\eta_{c,4.5\ K} = \frac{T_k}{T_w - T_K} = \frac{4,5\ K}{300\ K - 4,5\ K} = \frac{4,5\ K}{295,5\ K} = 0.01523$$

$$65.7\ W$$

4



What effort is required to cool back a heat output of 1 W at low temperatures?

Real efficiency of refrigerators

$$\eta_{real} = \eta_c \cdot COP$$

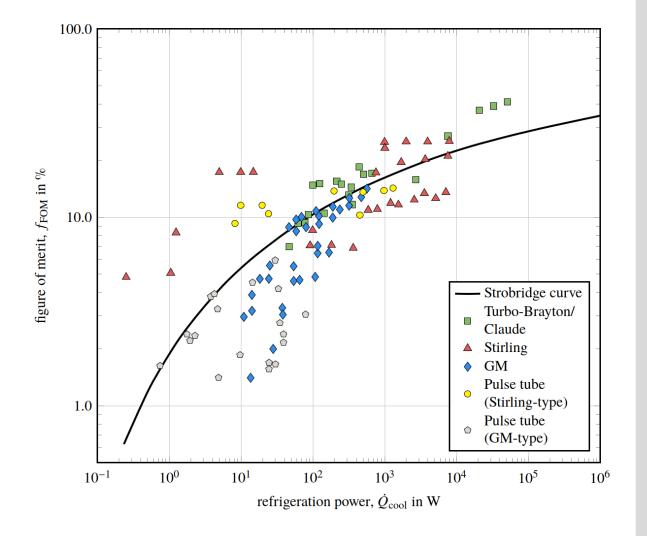
COP: Coefficient of Performance



What effort is required to cool back a heat output of 1 W at low temperatures?

Real efficiency of refrigerators

$$\eta_{real} = \eta_c \cdot COP$$





What effort is required to cool back a heat output of 1 W at low temperatures?

At 77 K

- 1 W heat load costs approx. 100 €/W for the purchase of the refrigeration plant
- 15-20 W electric power consumption per 1 W heat
- 1 Liter liquid nitrogen costs 10 ct to 1 € depending on purchase quantitiy

At 4,5 K

6

- 1 W heat load costs >1000 €/W for the purchase of the refrigeration plant
- 700-1000 W electric power consumption per 1 W heat
- 1 Liter liquid helium costs 10,6 € at KIT





What types of losses occur at low temperatures?

AC lesses Heat radiation Conduction Currentleals

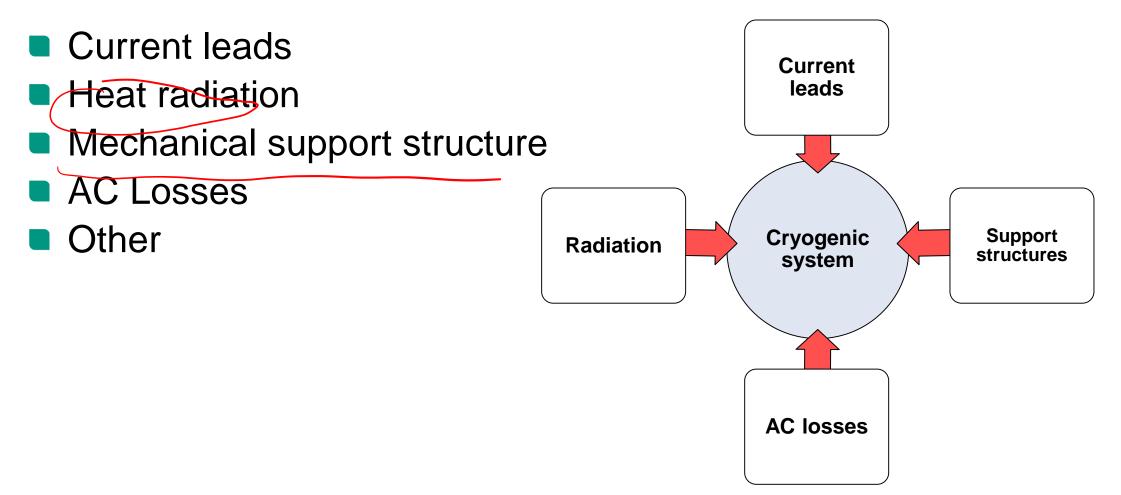
Motivation

7

9



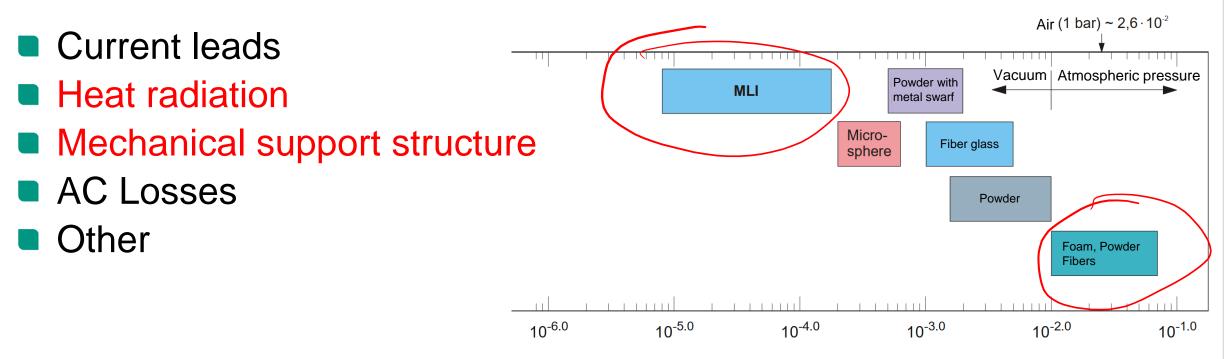
What types of losses occur at low temperatures?





10

What types of losses occur at low temperatures?



Thermal conductivity λ in W/(m*K) between 77 K – 300 K

Superinsulation - MLI

Karlsruhe Institute of Technology

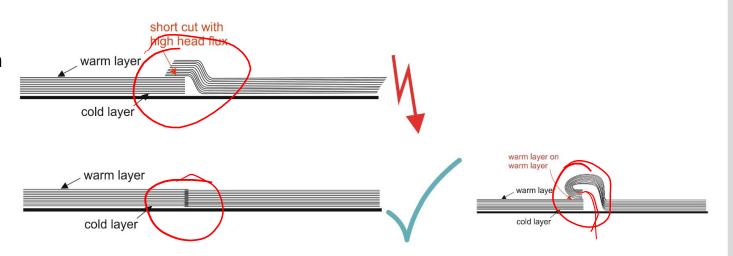
- Currently the most effective insulation method
- MLI consists of:
 - Reflective foils, coated polymer sheets
 - Reduction of heat radiation
 - Spacer between layers with minimal contact points
 - Reduction of heat conduction
 - High vacuum (10⁻³ 10⁻⁶ mbar)
 - Reduction of convection
 - Reduction of residual gas conduction

Requirements:

- High quality of materials
- Know-How

11

Careful processing





Contents

Motivation

Refrigerators

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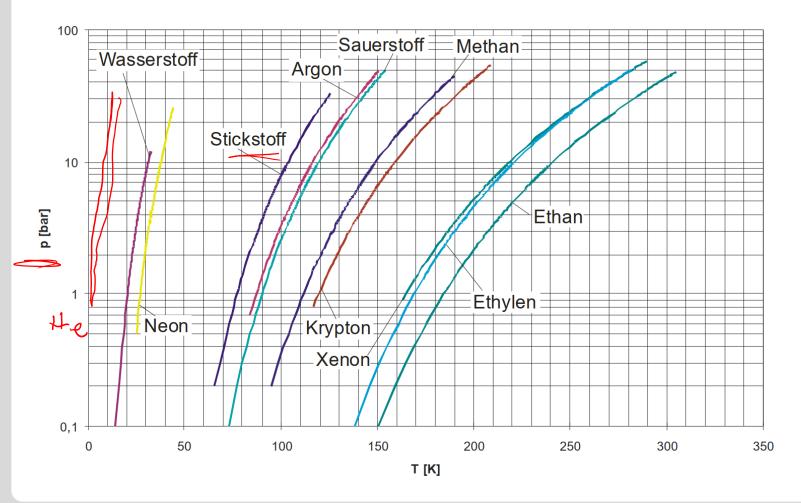
12

Application Examples

Pool boiling

13

Vapor pressure curves of cooling fluids





Pro

easy const. temperature

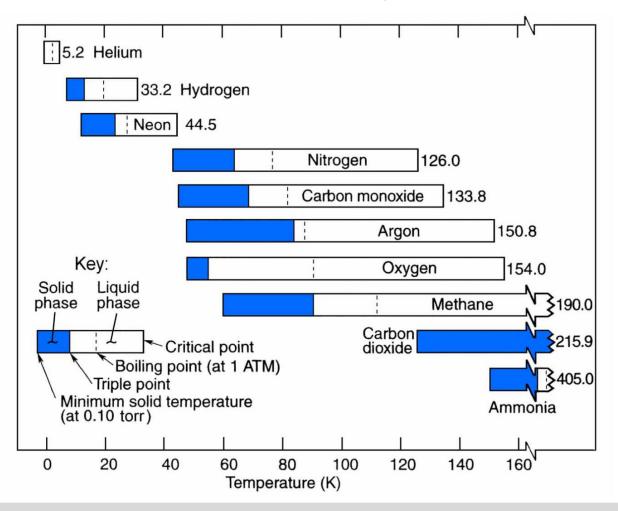
Con

temperature not freely gap between 30 K – 60 K refilling required

Pool boiling

14

Vapor pressure curves of cooling fluids





easy const. temperature

Con

Pro

temperature not freely gap between 30 K – 60 K refilling required

Nitrogen liquefication



Usually, liquid nitrogen is produced in large air separation plants.

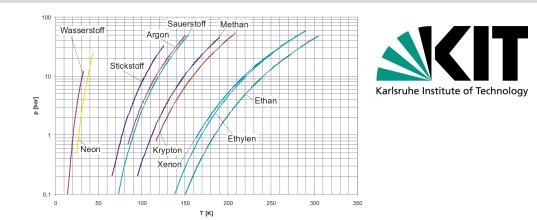


For a liquefaction capacity of 68 kg/h, 33 kWh of energy are required. (Data and pictures Friedhelm Herzog, Messer)

Pool boiling

16

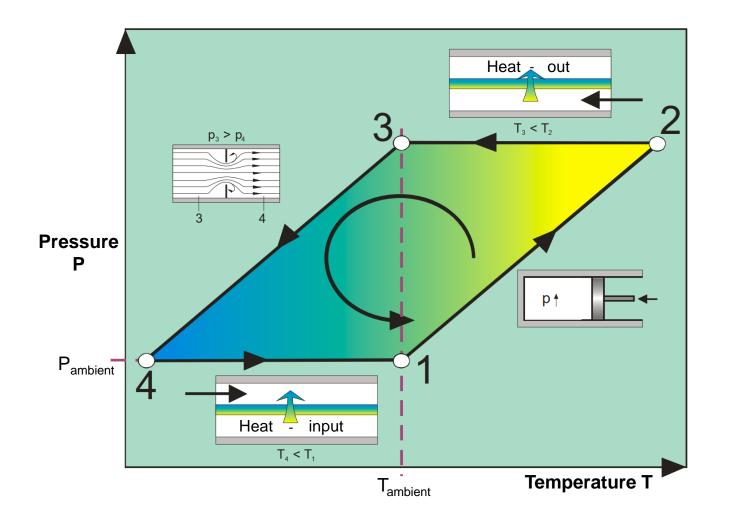
For which applications pool boiling under normal pressure can be used?



Cable	No, pressure difference needed
Current limiter	Yes, up to medium voltage (insulation)
Rotating machine	Yes, nearly normal pressure
Transformer	Yes, up to medium voltage (insulation)
SMES	Yes

Basic principle of refrigeration

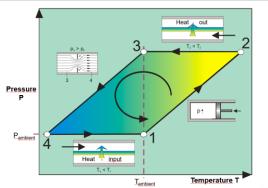




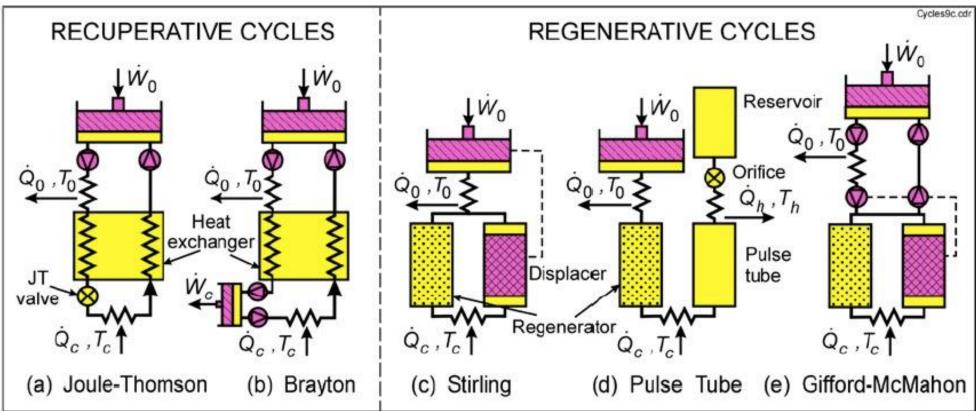
17

Refrigerators

Cryocooler types







Quelle: Radebough, J. Phys. Cond. Matter 21 (2009), 164219

Cryocooler



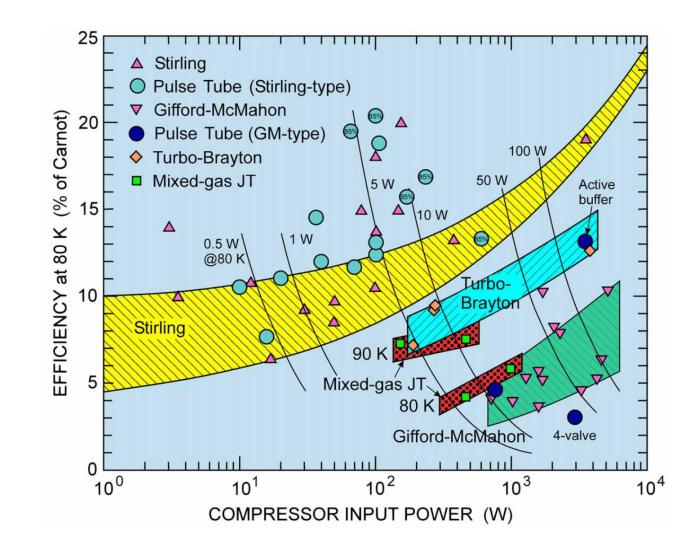
Principles

Туре	Explanation
Brayton	Turbines are used to compress a working gas, which is then expanded by either a turbine (Brayton) or a throttle (Joule-Thompson). The technology is particularly suitable for high outputs, e.g. in air condensers. For small Brayton systems, high speeds are required in the expander turbine, which make the technology more expensive.
Gifford- McMahon	This is a simplified variant of the Stirling process. Compressed gas is supplied via a compressor and the expansion volume is pressurized with high or low pressure via a rotary valve.
Pulse Tube	Pulse tube cooler is a refrigerating machine based on the principle of the Stirling engine. The advantage over the Stirling engine is that no mechanical moving parts are necessary near the cold heat exchange point. This makes very compact cooling heads possible and the achievable minimum temperature is not limited by the mechanical frictional heat of these parts.

Cryocooler

COP

Karlsruhe Institute of Technology





Overview Cryocooler

Overview of available cryocoolers > 100 W at 77 K

			Cooling		
Company	Cooling Type	Туре	Power	at Temp	Input Power
Sumitomo Heavy Industries	GM	CH 110	175 W	77 K	
Air Liquide	Turbo Brayton	TBF-80	7800 W	77 K	
Air Liquide	Turbo Brayton	TBF-175	16500 W	77 K	
Mayekawa	Turbo Brayton	Neo	5000 W	77 K	62,8 kW
Leybold	GM	Coolpower 250 MD	175 W	80 K	
Leybold	GM	Coolpower 140 T	140 W	80 K	
Fabrum Solutions	Pulse Tube	PTC 1000	1450W	77 K	25,0 kW
Fabrum Solutions	Pulse Tube	PTC 330	480 W	77 K	11,0 kW
Cryomech	Pulse Tube	РТ90	90 W	80 K	4,3 kW
Cryomech	GM	AL300	320 W	80 K	7,5 kW
Cryomech	GM	AL600	600 W	80 K	11,5 kW
Stirling	Reversed Stirling Cycle	SPC-1	1000 W	80 K	11,2 kW
Stirling	Reversed Stirling Cycle	SPC-4	4200 W	80 K	



Overview Cryocooler

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Air Liquide	Turbo Brayton	TBF-175	16500 W	77 K	
Mayekawa	Turbo Brayton	Brayton Neo	5000 W	77 K	62,80 kW
Leybold	GM	Coolpower 250 MD	175 W	80 K	
Leybold	GM	Coolpower 140 T	140 W	80 K	
Fabrum Solutions	Pulse Tube	PTC 1000	1450 W	77 K	25,00 kW
Fabrum Solutions	Pulse Tube	PTC 330	480 W	77 K	11,00 kW
Cryomech	Pulse Tube	РТ90	90 W	80 K	4,30 kW
Cryomech	GM	AL300	320 W	80 K	7,50 kW
Cryomech	GM	AL600	600 W	80 K	11,50 kW
Stirling	Reversed Stirling Cycle	SPC-1	1000 W	80 K	11,20 kW
Stirling	Reversed Stirling Cycle	SPC-4	4200 W	80 K	

Examples Cryocooler



Cryomech AL 600 (GM)

:
,

600W @ 80K, 500 W @ 70 K 15 Min to 80K 41.8kg CPA1114 470lb (213kg) 61 X 61 X 79cm 380/415 VAC 3 PH / 11.5kW Water (11,4 l/min) or air 7 to 38°C



Examples Cryocooler



Fabrum PTC 1000 (PT Stirling)

Cooling capacity	1450 W @ 77 K
Input power	25 kW
Weight	1300 kg
Cooling	Water (40 l/min) or air
Dimensions	1.8 (L) x 1.2 (W) x 2.1(H) m
Temperature range:	0 to 35°C
Buffer Volume	

30 kW motor ABB-M3AA200MLA-2 B5





Oil reser

Examples Cryocooler



Mayekawa Brayton NeO

Cooling capacity Input power Weight Cooling Dimensions COP 5000 W at 77 K 75 kW 5.500 kg Water 200 l/min 2,2x3,6x2,2 m 0.08 @ 77 K





Contents

Motivations

Refrigerator

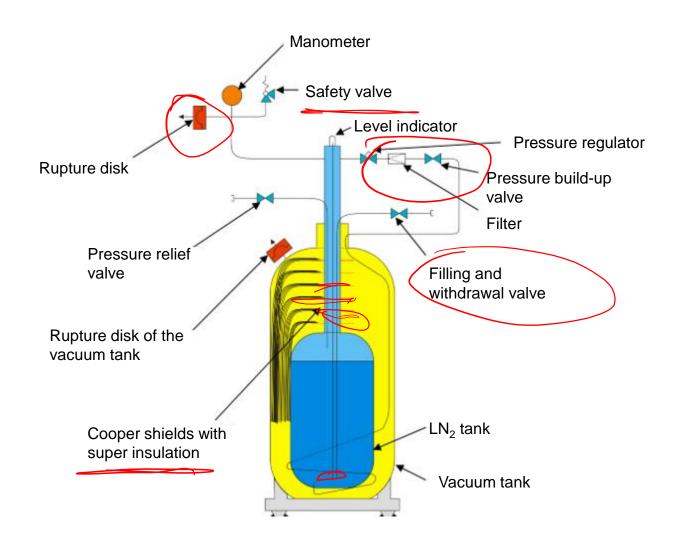
Cryostats

26

Application Examples

Schematic sketch of a LN₂ cryostat





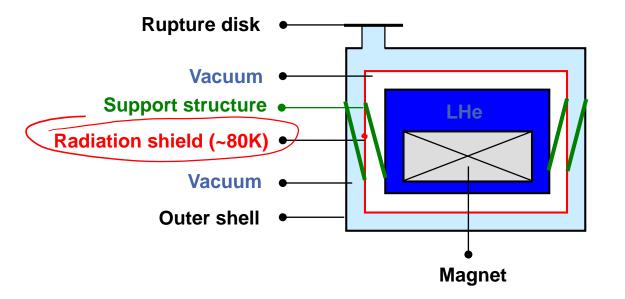


27



Schematic sketch LHe cooled magnet

Cryostat with liquid helium

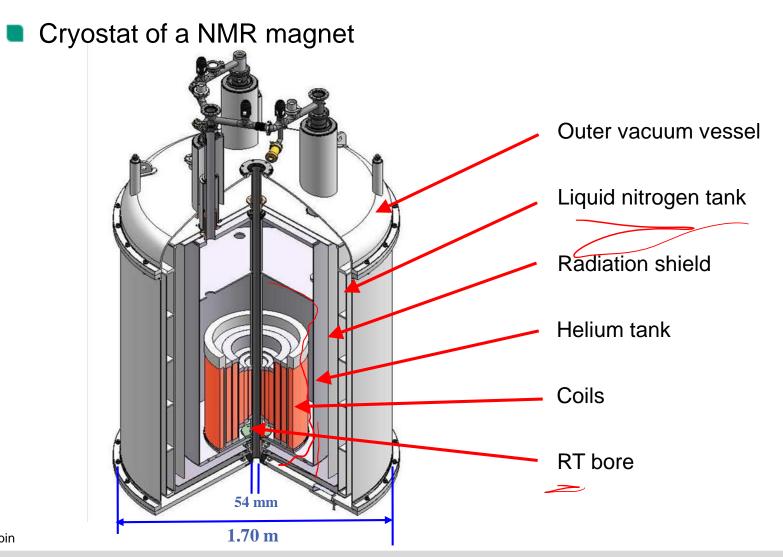


Thermal cryostat losses

- Thermal conduction through support structure
- Thermal radiation from warm to cold surfaces
- Residual gas thermal conduction
- Current lead losses and sensor lines

Application example





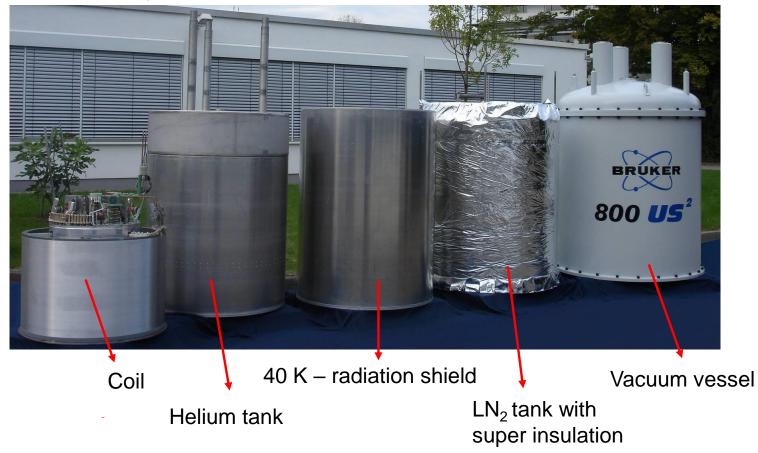
Source: Bruker Biospin



Application example

Cryostat of a NMR magnet

Picture: Bruker Biospin





Contents

Motivations

Refrigerator

Cryostats

32

Application Examples

1,000 m

10,000 V

4 kW

- 206°C

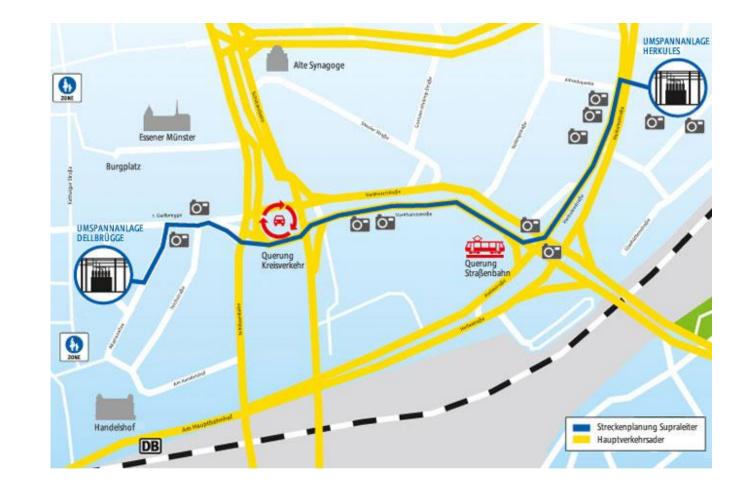
(67 K)

40,000 kW

Project data

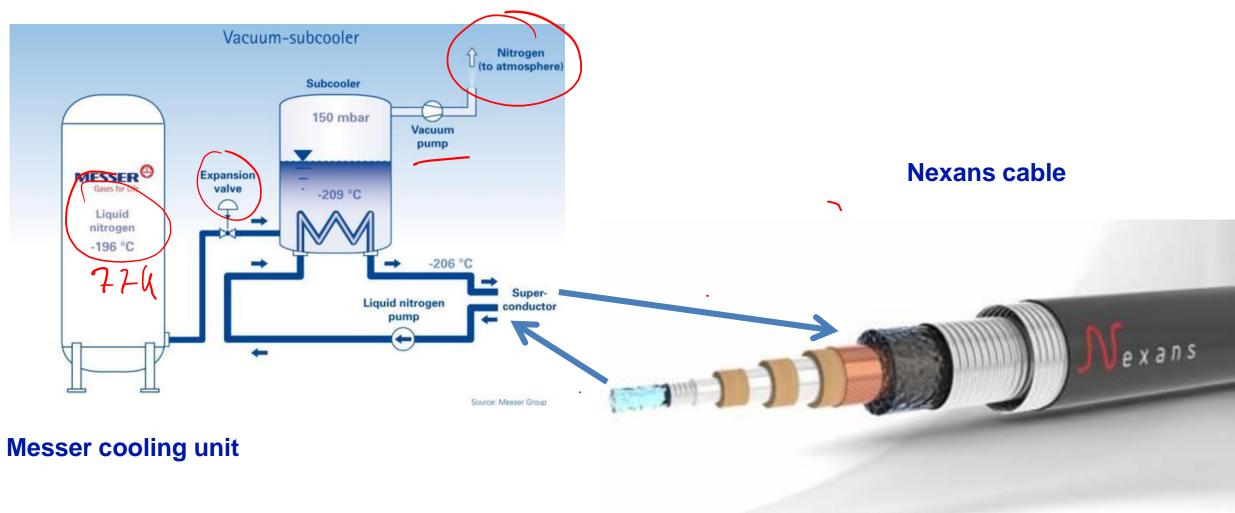
Place: Essen, Germany

- Cable length:
- Voltage:
- Electrical capacity:
- Cooling capacity (cable):
- Cooling temperature:





The most important components

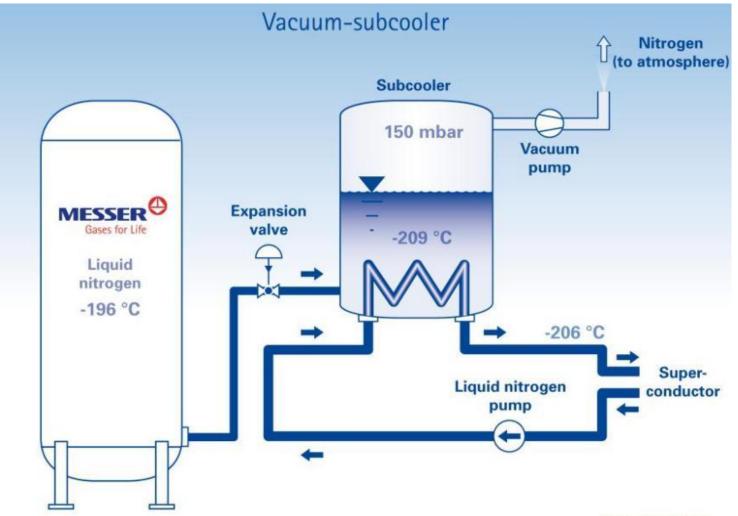




HTS – cooling unit

Basic diagram

- Liquid nitrogen is used
 - as heat transfer medium
 - as cooling agent
- LIN is pumped through the superconducting cable
- LIN is recooled in the subcooler (to -206°C)
- LIN vaporizes at 150 mbar(a) (forced by vacuum pumps)
- LIN temperature decreases to -209°C (expansion through the regulation valve)

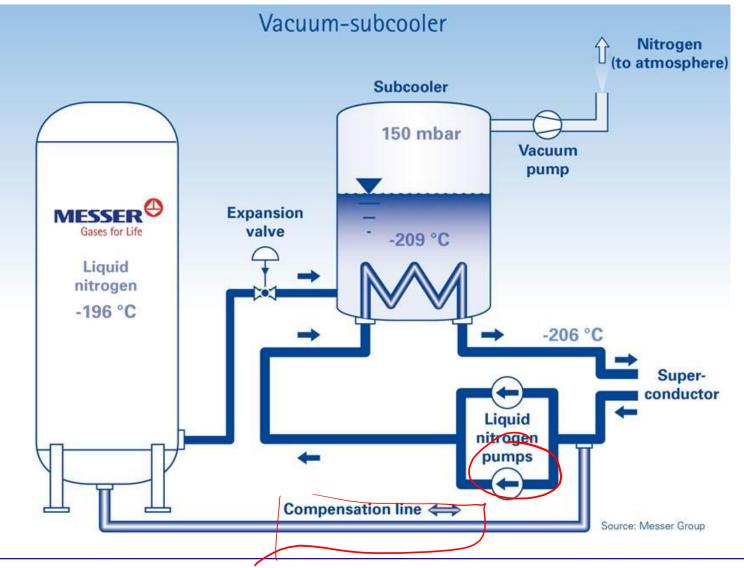


Source: Messer Group



Redundancy (circulation)

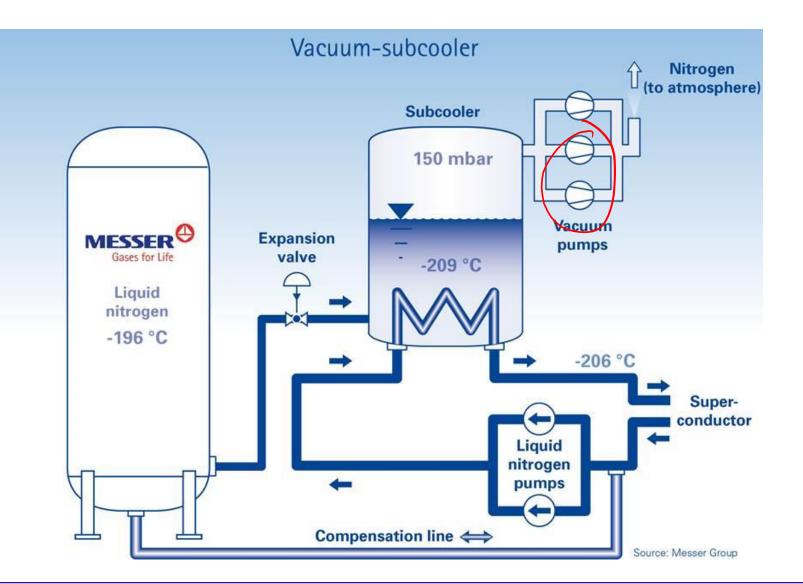
- There are installed 2 liquid nitrogen circulation pumps.
- 1 pump is in operation, the other one is in standby.
- Pump maintanance is done without stopping the circuit.
- In case of malfunction there is automatic switchover to the standby pump.
- Full redundancy for the circulation is achived with quite low additional investment (app. 3%).





Redundancy (vacuum pumps)

- For operation at full capacity (4 kW @ 67 K) 2 vacuum pumps are in operation.
- In case of failure the duty of the malfunctioning item is automatically taken over by the 3rd vacuum pump.
 (app. 1% add. investment)
- For operation at actual capacity (1.8 kW @ 67 K) only 1 vacuum pump is necessary.
- Actual 2 vacuum pumps are in reserve.





HTS – cooling unit

Photo of the cooling unit during FAT - 09.10.2013 -(factory acceptance test)

- Left: control cabinet
- Bottom (blue): LIN pumps
- Right: vacuum pump skid





Tank Installation

- 19.09.2013
- Transport
- Installation and piping





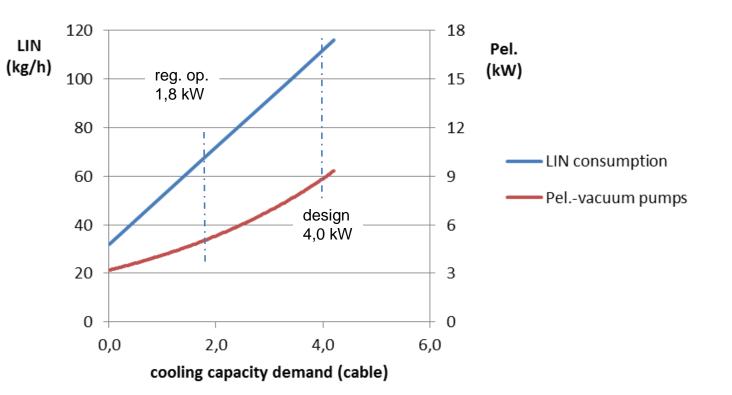


	cooling- demand (cable)	liquid nitrogen consumption	P _{el.} vacuum pumps	P _{el.} other components	P _{el.} total
design	4.0 kW	110 kg/h	9 kW		13 kW
regular operation	1.8 kW	68 kg/h	5 kW	4 kW	9 kW
cable-bypassed	0.0 kW	32 kg/h	3 kW		7 kW



Cable-cooling demand:

design 4.0 kW
regular operation 1.8 kW
cable-bypass 0.0 kW





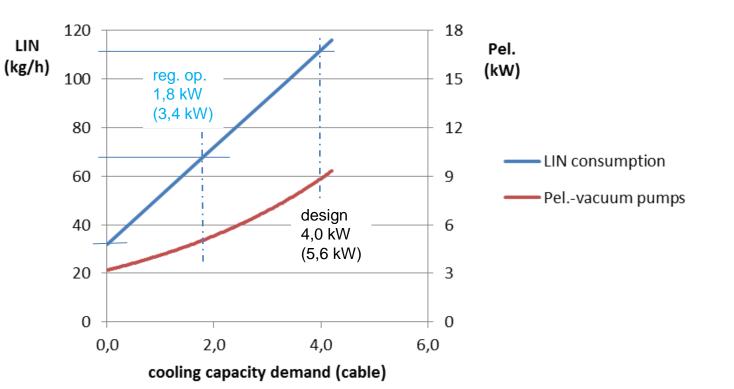
Cable-cooling demand:

design 4.0 kW
regular operation 1.8 kW
cable-bypass 0.0 kW

total-required cooling capacity:

- design (5.6 kW)
- regular operation
- cable-bypass

(3.4 kW) (1.6 kW)





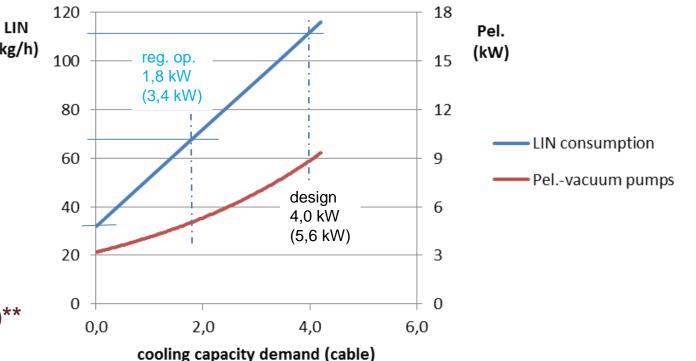
Cable-cooling demand:

- design 4.0 kW @ 67 K
- regular operation 1.8
- cable-bypass

total-required cooling capacity:

- design (5.6 kW) @ 64 K
- regular operation (3.4
- cable-bypass

(3.4 kW) (- 209°C)** (1.6 kW)



** N2 becomes solid at 63 K (-210°C)



Energy-data comparison (regular operation point)

- Cable-cooling demand:
- Total required cooling capacity:
- Liquid nitrogen consumption:

1.8 kW (@ 67 K) 3.4 kW (@ 64 K)

68 kg/h



air separation unit (ASU)

➔ transport

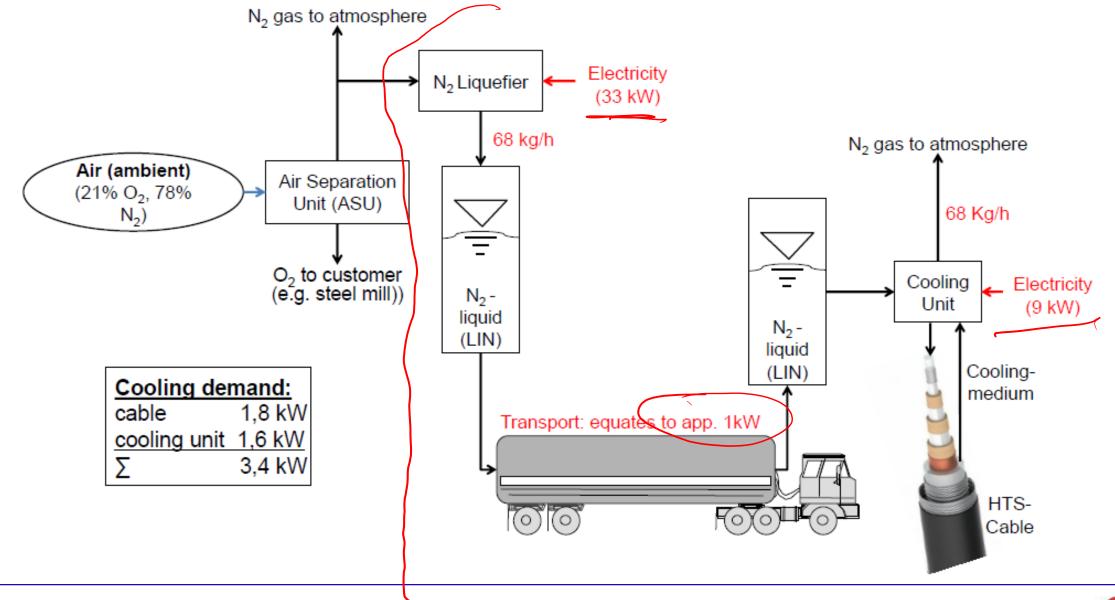
tank

→ cooling unit





HTS – cooling unit: nitrogen and energy balance





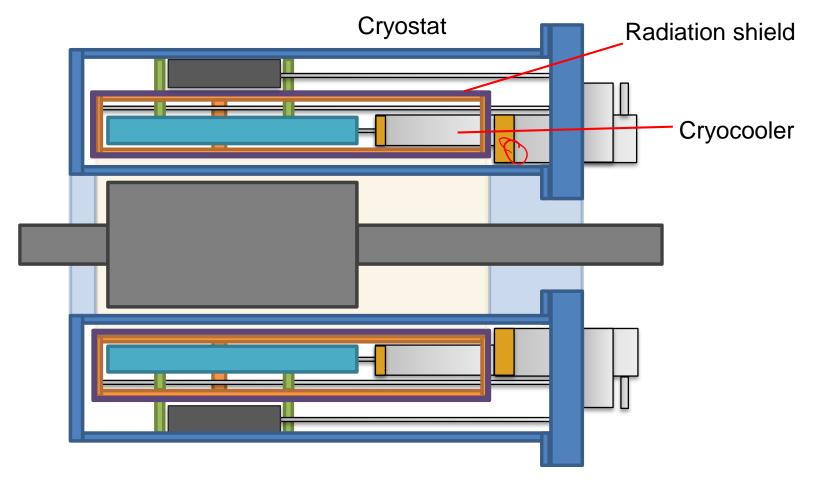
Energy-data comparison (regular operation point)

 Cable-cooling demand: 	1.8 kW (@ 67 K)	CASE CONTRACTOR
 Total required cooling capacity: 	3.4 kW (@ 64 K)	
 Liquid nitrogen consumption: 	68 kg/h	
 Required electricity for N2-liquefying: 	33 kW	
 Exergetic effect LIN transport (130 km)): 1 kW	
 Pel. (vacuum pumps): 	5 kW	
Pel. (other equipment):	<u>4 kW</u>	
total:	43 kW	
 for comparison: 	IN THE DOLLAR OF MEXA	
Pel. for mechanical cooling: 75 to (dependant on the availability of cooling)	o 100 kW ng water)	



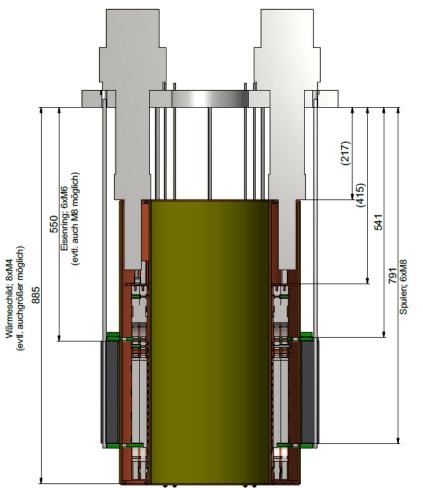


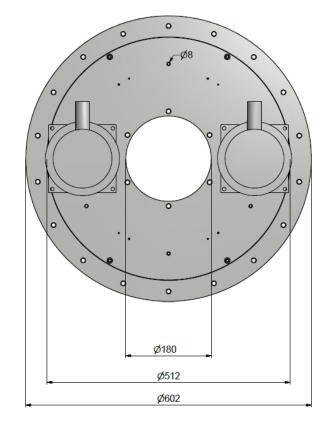
PhD thesis Fabian Schreiner





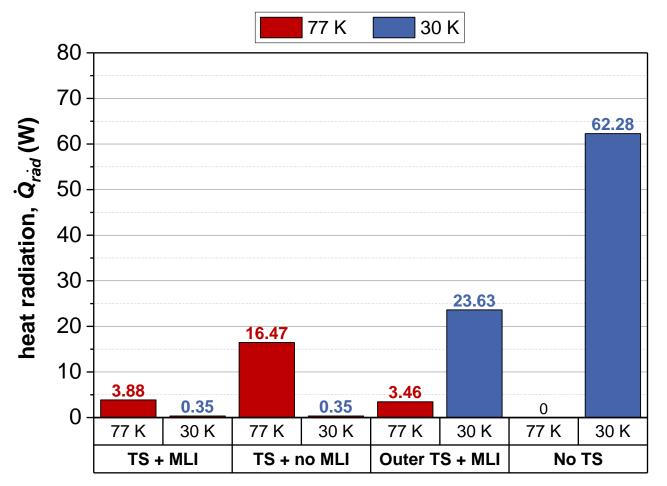






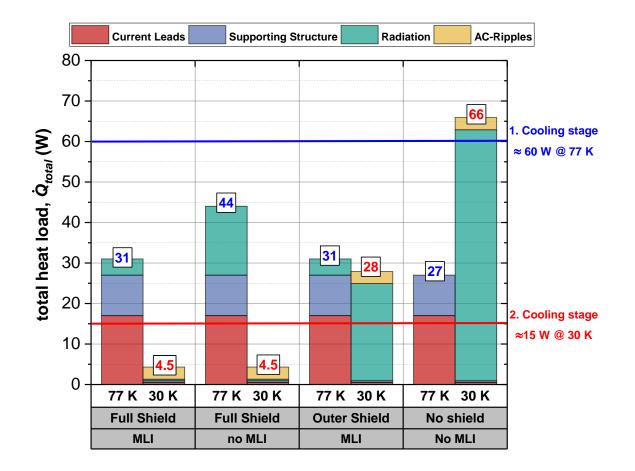


PhD thesis Fabian Schreiner





Comparison of total heat input with 4 mm Theva tape





Comparison of total heat input with 12 mm Theva tape

